COMPUTATIONAL FLUID DYNAMICS MODELING OF THERMO-CHEMICAL PROCESSES IN AN UPDRAFT BIOMASS GASIFIER

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Thesis submitted in partial fulfillment of the requirements for the Degree Master of Science

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DECLARATION OF THE CANDIDATE AND SUPERVISOR

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ABSTRACT

Biomass is recently gaining popularity in industry as a promising source of renewable energy. Gasification of biomass is a major thermal conversion method to improve the efficiency of raw biomass fuel. It is a process by which biomass is partially oxidized to produce a combustible gas named Syngas; a mixture of carbon monoxide, hydrogen and methane. Although the gasification technology is used throughout the history and there are a large number of gasification plants worldwide, their smooth operation remains questionable. This is due to a lack of understanding of proper design criteria. In order to gain insights to optimal design parameters, mathematical models and computer simulations based performance analysis can be used. Recently Computational Fluid Dynamics (CFD) analysis has been applied by many researchers as a tool for optimizing packed bed processes including gasification process. In this research study, a two dimensional CFD model has been developed for an updraft biomass gasifier. The model uses air as the gasifying medium and a fixed batch of biomass. The model is capable of tracking the movement of interface between solid packed bed and gas free board due to bed shrinkage. The two phase model is developed using the Euler-Euler approach. The model consists of several sub models, including reaction models, turbulence model for packed bed gas phase and free board, a radiation model for solid phase, a bed shrinkage model, and interphase heat transfer models. The final mathematical model is converted into a numerical model using open source CFD tool OpenFOAM. Required code was developed by using C++ language in OpenFOAM package, including all the relevant differential equations and procedures in the CFD model. To validate the CFD model, simulation results for gas temperature and gas compositions are compared against experimental gas temperatures and compositions measured from an operational laboratory gasifier. The validated model is used to perform air flow rate optimization. A series of CFD simulations were performed for air flow rates ranging from 3 m^3 /hr to 10 m^3 /hr for a computational geometry corresponding to the experimental gasifier and cumulative CO was calculated. It is found that cumulative CO production maximized at 7 m³/hr airflow rate. The maximum cumulative CO volume was 6.4 m³.

Keywords: Biomass, Gasification, Mathematical Model, Computational Fluid Dynamics

DEDICATION

This thesis is dedicated to my beloved mother and to the loving memory of my father



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NOMENCLATURE

Α	Specific surface area of packed bed (m ⁻¹)	$r_{i,homo}$	Rate of homogenous reaction i
4			$(\text{Kg m}^{-3} \text{ s}^{-1})$
A _c	Specific surface area of char (m)	$r_{m,i}$	(Kg m ⁻³ s ⁻¹) (Kg m ⁻³ s ⁻¹)
A_d	Specific surface area for gas diffusion (m ⁻¹)	$r_{k,i}$	Kinetic reaction rate (Kg m ⁻³ s ⁻¹)
A_{a}	Cross sectional area of gasifier (m ²)	$r_{t,i}$	Turbulent mixing limited reaction
3		-,-	rate (kg $m^{-3} s^{-1}$)
A_j	pre-exponential factor for heterogeneous reactions $(m s^{-1} T^{-1})$	Sh _j	Sherwood number for species j
A_r	Specific surface area available for radiation (m ⁻¹)	Sø	Source term for property Ø
а	Absorption coefficient of gas phase (m ⁻¹)	$S_{s,\emptyset}$	Source term for property \emptyset due to solid phase
a_p	Absorption coefficient of solid phase (m ⁻¹)	$S_{g,\emptyset}$	Source term for property \emptyset due to gas phase
C_{q}	Heat capacity of gas phase (J kg ⁻¹ K ⁻¹)	S _{ii}	Reynolds stress tensor (Pa)
$\tilde{C_s}$	Heat capacity of solid phase (J kg ⁻¹ K ⁻¹)	T_{a}	Gas phase temperature (K)
$D_{i,a}$	Diffusion coefficient of gas species i $(m^2 s^{-1})$	$T_{a,in}$	Inlet gas temperature (K)
d	Particle size of biomass (m)	$T_{\rm s}$	Solid phase temperature (K)
E_i	Activation energy of reaction i (J mol ⁻¹)	Ŭ _a	Gas phase velocity (m s ⁻¹)
f_i	Pre-exponential factor of reaction i (s ⁻¹)	$U_{a,in}$	Inlet gas velocity (m s ⁻¹)
G	Radiation intensity (W m^{-2})	U,	Shrinkage velocity $(m s^{-1})$
h	Heat transfer coefficient ($W m^{-2} K^{-1}$)	v_i	Stoichiometric coefficient of
		·	species i
k	Turbulent kinetic energy $(m^2 s^{-2})$	$Y_{i,g}$	Mole fraction of gas species i
k_g	Thermal conductivity of gas phase (Wm ⁻¹ K ⁻¹) W	a Kain I	Mole fraction of i in air
k _s	Thermal conductivity of solid phase (W m ⁻¹ K ⁻¹)	Yist	Mole fraction of solid species i
$k_{m,i}$	Wass transfer coefficient of species $f(ms^{-1})$	Isserial	Stefan constant ($W m^{-2} K^{-4}$)
Mi	Nietecular weighvol/species in kg.mol.1)k	σ_p	Scattering coefficient of solid
		Ł	particles (m ⁻¹)
m_i	Density of species i in a computational cell	ϵ	Emissivity of solid particles
	$({\rm kg \ m^{-3}})$		
Nu	Nusselt number	Ø	A general transport property
n	Refractive index of gas phase	\mathcal{E}_{g}	Gas phase fraction
Pr	Prandtl number	ε_s	Solid phase fraction
p	Pressure (Pa)	$ ho_g$	Density of gas phase (Kg m ⁻³)
p_{in}	Inlet pressure (Pa)	$ ho_s$	Density of solid phase (Kg m ⁻³)
Q_{rad}	Radiation heat source (W m ⁻³)	$ ho_j$	Cell density of species j (Kg m ⁻³)
Q_i	Initial heat source (W m ⁻³)	μ	Dynamic viscosity (Pa s)
Q_{sg}	Convective heat transfer rate (W m ⁻³)	$\sigma_{i,air}$	Average collision diameter (A)
q_r	Radiation heat flux (Wm ⁻²)	$\Omega_{i,air}$	Diffusion collision integral
Re	Reynolds number	ε	Turbulent dissipation rate (m ² s ⁻³)
$R_{g,pyro}$	2 1		
	Rate of release of pyrolytic volatiles (Kg m ⁻³ s ⁻¹)	ΔH_i	Enthalpy of reaction i (J kg ⁻¹)
r_i	Rate of release of pyrolytic volatiles (Kg m ⁻³ s ⁻¹) Rate of reaction i (Kg m ⁻³ s ⁻¹)	ΔH_i	Enthalpy of reaction i (J kg ⁻¹) Vector outer product

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Appendix OpenFOAM Case Settings

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